

## ACPL-331J

### 1.5A Output Current IGBT Gate Driver Optocoupler with Integrated ( $V_{CE}$ ) Desaturation Detection, UVLO, Fault Status Feedback, and Active Miller Clamping

#### Overview

The Broadcom® ACPL-331J is an advanced 1.5A output current, easy-to-use, intelligent gate driver that makes IGBT  $V_{CE}$  fault protection compact, affordable, and easy to implement. Features such as integrated  $V_{CE}$  detection, under-voltage lockout (UVLO), *soft* IGBT turn-off, isolated open collector fault feedback, and active Miller clamping provide maximum design flexibility and circuit protection.

The ACPL-331J contains an AlGaAs LED. The LED is optically coupled to an integrated circuit with a power output stage. The ACPL-331J is ideally suited for driving power IGBTs and MOSFETs used in motor control inverter applications. The voltage and current supplied by this optocoupler make it ideally suited for directly driving IGBTs with ratings up to 1200V and 100A. For IGBTs with higher ratings, the ACPL-331J can be used to drive a discrete power stage that drives the IGBT gate. The ACPL-331J has an insulation voltage of  $V_{IORM} = 1414 V_{PEAK}$ .

#### Applications

- Isolated IGBT/Power MOSFET gate drive
- AC and brushless DC motor drives
- Industrial inverters and uninterruptible power supply (UPS)

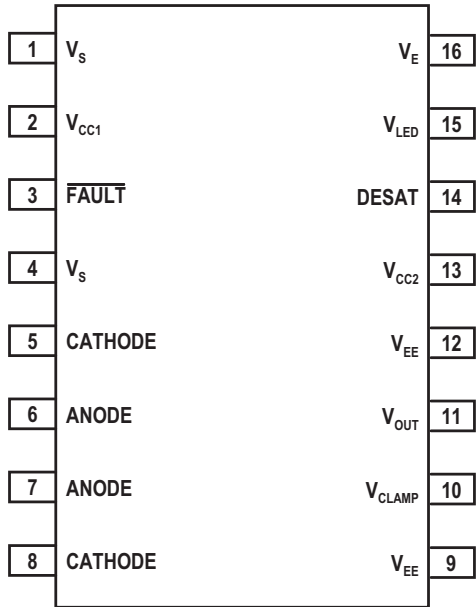
#### Features

- 1.5A maximum peak output current
- 1.0A minimum peak output current
- 250-ns maximum propagation delay over temperature range
- 1.0A Miller clamp (Clamp pin short to  $V_{EE}$  if not used.)
- Under-voltage lockout (UVLO) with hysteresis
- Desaturation detection
- Open collector isolated fault feedback
- *Soft* IGBT turn-off
- Fault reset by next LED turn-on (low to high) after fault mute period
- Available in SO-16 package
- 100-ns maximum pulse width distortion (PWD)
- 50-kV/ $\mu$ s minimum common mode rejection (CMR) at  $V_{CM} = 1500V$
- $I_{CC(max)} < 5$  mA maximum supply current
- Wide  $V_{CC}$  operating range: 15V to 30V over temperature range
- Wide operating temperature range:  $-40^{\circ}C$  to  $105^{\circ}C$
- Safety approvals:
  - UL approved, 5000  $V_{RMS}$  for 1 minute
  - CSA approved
  - IEC/EN/DIN-EN 60747-5-5 approved $V_{IORM} = 1414 V_{PEAK}$

**CAUTION!** Take normal static precautions in handling and assembly of this component to prevent damage and degradation that might be induced by electrostatic discharge (ESD). The components featured in this data sheet are not designed to be used in military or aerospace applications or environments.

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Pin Description



Pin	Symbol	Description
1	V <sub>S</sub>	Input ground.
2	V <sub>CC1</sub>	Positive input supply voltage (3.3V to 5.5V).
3	FAULT	Fault output. FAULT changes from a high impedance state to a logic low output within 0.5 μs of the voltage on the DESAT pin exceeding an internal reference voltage of 6.5V. FAULT is an open collector output that allows the FAULT outputs from all ACPL-331J in the circuit to be wired OR together. This forms a single fault bus for interfacing directly to the microcontroller.
4	V <sub>S</sub>	Input ground.
5	CATHODE	Cathode.
6	ANODE	Anode.
7	ANODE	Anode.
8	CATHODE	Cathode.
9	V <sub>EE</sub>	Output supply voltage.
10	V <sub>CLAMP</sub>	Miller clamp.
11	V <sub>OUT</sub>	Gate drive voltage output.
12	V <sub>EE</sub>	Output supply voltage.
13	V <sub>CC2</sub>	Positive output supply voltage.
14	DESAT	Desaturation voltage input. When the voltage on DESAT exceeds an internal reference voltage of 6.5V while the IGBT is on, the FAULT output is changed from a high impedance state to a logic low state within 0.5 μs.
15	V <sub>LED</sub>	LED anode. This pin must be left unconnected for guaranteed data sheet performance. (For optical coupling testing only.)
16	V <sub>E</sub>	Common (IGBT emitter) output supply voltage.

## Ordering Information

ACPL-331J is UL recognized with 5000  $V_{RMS}$  for 1 minute per UL1577.

Part Number	Option (RoHS Compliant)	Package	Surface Mount	Tape and Reel	IEC/EN/DIN EN 60747-5-5	Quantity
ACPL-331J	-000E	SO-16	X		X	45 per tube
	-500E		X	X	X	850 per reel

To order, choose a part number from the part number column and combine with the desired option from the option column to form an order entry.

### Example 1:

ACPL-331J-500E to order product of SO-16 surface-mount package in tape and reel packaging with IEC/EN/DIN EN 60747-5-5 safety approval in RoHS compliant.

### Example 2:

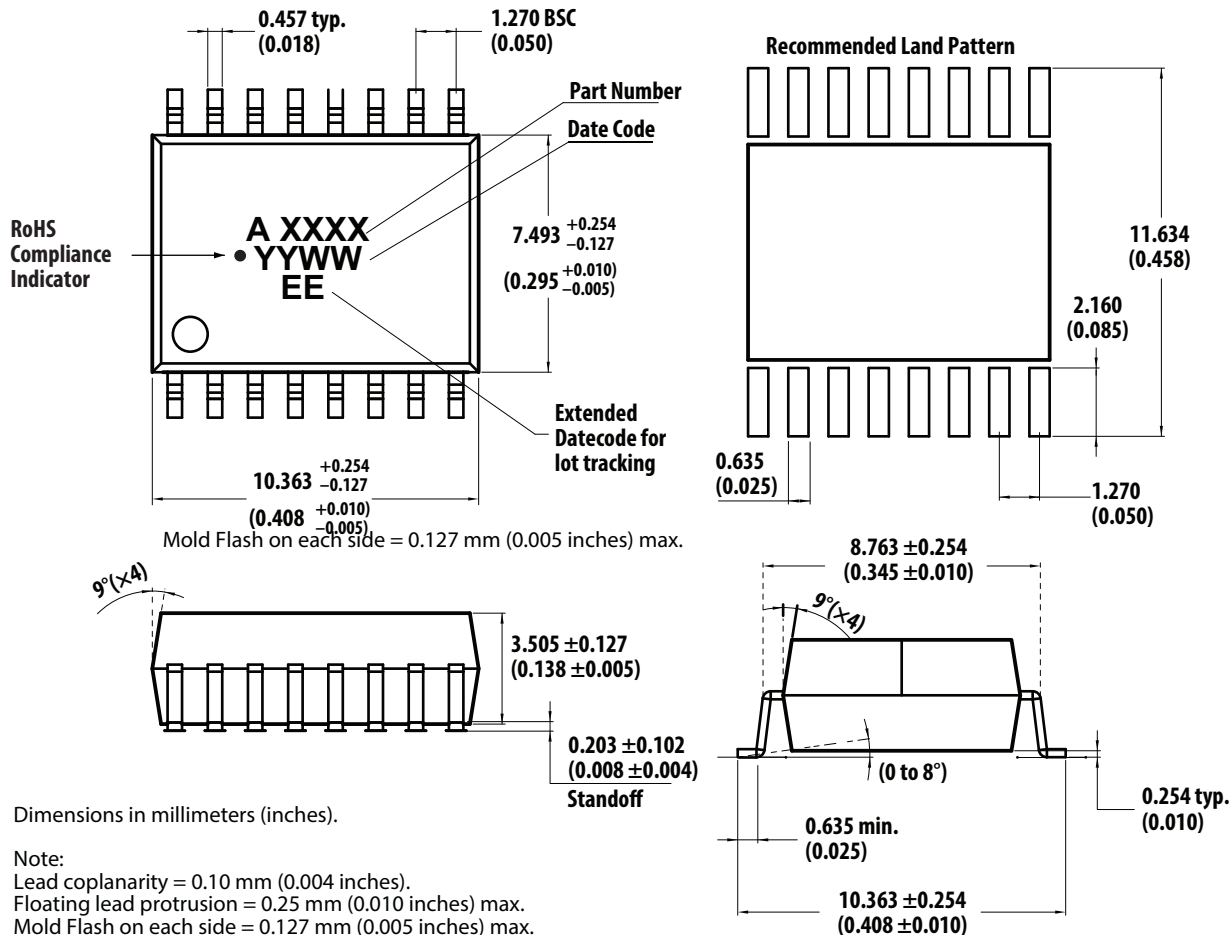
ACPL-331J-000E to order product of SO-16 surface-mount package in tube packaging with IEC/EN/DIN EN 60747-5-5 safety approval and RoHS compliant

Option data sheets are available. Contact your Broadcom sales representative or authorized distributor for information.

**NOTE:** The notation #XXX is used for existing products, while (new) products launched since 15th July 2001 and RoHS compliant option will use -XXXE.

## Package Outline Drawing

### SO-16 Surface-Mount Package



## Recommended Pb-Free IR Profile

Recommended reflow condition as per JEDEC Standard, J-STD-020 (latest revision). Non-halide flux should be used.

## Regulatory Information

The ACPL-331J is approved by the following organizations:

IEC/EN/DIN EN 60747-5-5	Approval under IEC 60747-5-5, DIN EN 60747-5-5, EN 60747-5-5.
UL	Approval under UL 1577, component recognition program up to $V_{ISO} = 5000 V_{RMS}$ . File E55361.
CSA	Approval under CSA Component Acceptance Notice #5, File CA 88324.

## IEC/EN/DIN EN60747-5-5 Insulation Characteristics

**NOTE:** Isolation characteristics are guaranteed only within the safety maximum ratings, which must be ensured by protective circuits in application. Surface-mount classification is class A in accordance with CECC 00802.

Description	Symbol	Characteristic	Unit
Insulation Classification per DIN VDE 0110/1.89, Table 1			
For Rated Mains Voltage $\leq 150 V_{RMS}$		I – IV	
For Rated Mains Voltage $\leq 300 V_{RMS}$		I – IV	
For Rated Mains Voltage $\leq 600 V_{RMS}$		I – IV	
For Rated Mains Voltage $\leq 1000 V_{RMS}$		I – III	
Climatic Classification		40/100/21	
Pollution Degree (DIN VDE 0110/1.89)		2	
Maximum Working Insulation Voltage	$V_{IORM}$	1414	$V_{PEAK}$
Input to Output Test Voltage, Method b <sup>a</sup> $V_{IORM} \times 1.875 = V_{PR}$ , 100% Production Test with $t_m = 1$ second, Partial Discharge $< 5$ pC	$V_{PR}$	2652	$V_{PEAK}$
Input to Output Test Voltage, Method a <sup>a</sup> $V_{IORM} \times 1.6 = V_{PR}$ , Type and Sample Test, $t_m = 10$ seconds, Partial Discharge $< 5$ pC	$V_{PR}$	2262	$V_{PEAK}$
Highest Allowable Overvoltage (Transient Overvoltage $t_{ini} = 60$ seconds)	$V_{IOTM}$	8000	$V_{PEAK}$
Safety-Limiting Values (Maximum values allowed in the event of a failure)			
Case Temperature	$T_S$	175	$^{\circ}C$
Input Current	$I_{S,INPUT}$	400	mA
Output Power	$P_{S,OUTPUT}$	1200	mW
Insulation Resistance at $T_S$ , $V_{IO} = 500V$	$R_S$	$> 10^9$	$\Omega$

a. Refer to IEC/EN/DIN EN 60747-5-5 Optoisolator Safety Standard section of the *Broadcom Regulatory Guide to Isolation Circuits*, AV02-2041EN, for a detailed description of Method a and Method b partial discharge test profiles.

## Insulation and Safety Related Specifications

Parameter	Symbol	Value	Unit	Conditions
Minimum External Air Gap (Clearance)	L(101)	8.3	mm	Measured from input terminals to output terminals, shortest distance through air.
Minimum External Tracking (Creepage)	L(102)	8.3	mm	Measured from input terminals to output terminals, shortest distance path along body.
Minimum Internal Plastic Gap (Internal Clearance)		0.5	mm	Through insulation distance conductor to conductor, usually the straight line distance thickness between the emitter and detector.
Tracking Resistance (Comparative Tracking Index)	CTI	$>175$	V	DIN IEC 112/VDE 0303 Part 1
Isolation Group		IIIa		Material Group (DIN VDE 0110, 1/89, Table 1)

## Absolute Maximum Ratings

Parameter	Symbol	Min.	Max.	Unit	Note
Storage Temperature	$T_S$	-55	125	°C	
Operating Temperature	$T_A$	-40	105	°C	a
Output IC Junction Temperature	$T_J$	—	125	°C	a
Average Input Current	$I_{F(AVG)}$	—	25	mA	b
Peak Transient Input Current (<1 $\mu$ s pulse width, 300 pps)	$I_{F(TRAN)}$	—	1.0	A	
Reverse Input Voltage	$V_R$	—	5	V	
High Peak Output Current	$I_{OH(PEAK)}$	—	1.5	A	c
Low Peak Output Current	$I_{OL(PEAK)}$	—	1.5	A	c
Positive Input Supply Voltage	$V_{CC1}$	-0.5	7	V	
$\overline{FAULT}$ Output Current	$I_{\overline{FAULT}}$	—	8.0	mA	
$\overline{FAULT}$ Pin Voltage	$V_{\overline{FAULT}}$	-0.5	$V_{CC1}$	V	
Total Output Supply Voltage	$(V_{CC2} - V_{EE})$	-0.5	35	V	
Negative Output Supply Voltage	$(V_E - V_{EE})$	-0.5	15	V	d
Positive Output Supply Voltage	$(V_{CC2} - V_E)$	-0.5	$35 - (V_E - V_{EE})$	V	
Gate Drive Output Voltage	$V_{O(PEAK)}$	-0.5	$V_{CC2}$	V	
Peak Clamping Sinking Current	$I_{CLAMP}$	—	1.0	A	
Miller Clamping Pin Voltage	$V_{CLAMP}$	-0.5	$V_{CC2}$	V	
DESAT Voltage	$V_{DESAT}$	$V_E$	$V_E + 10$	V	
Output IC Power Dissipation	$P_O$	—	600	mW	a
Input IC Power Dissipation	$P_I$	—	150	mW	a
Solder Reflow Temperature Profile	See <a href="#">Package Outline Drawing</a> section.				

- To achieve the absolute maximum power dissipation specified, pins 4, 9, and 10 require ground plane connections and might require airflow. See the [Thermal Model](#) section for details about how to estimate junction temperature and power dissipation. In most cases, the absolute maximum output IC junction temperature is the limiting factor. The actual power dissipation achievable will depend on the application environment (PCB layout, airflow, part placement, and so on). Output IC power dissipation is derated linearly at 10 mW/°C above 90°C. Input IC power dissipation does not require derating.
- Derate linearly above 70°C free-air temperature at a rate of 0.3 mA/°C.
- Maximum pulse width = 10  $\mu$ s. This value is intended to allow for component tolerances for designs with  $I_O$  peak minimum = 1.0A. Derate linearly from 2.0A at +25°C to 1.5A at +105°C. This compensates for increased  $I_{OPEAK}$  due to changes in  $V_{OL}$  over temperature.
- See the [Slow IGBT Gate Discharge during Fault Condition](#) section for further details.

## Recommended Operating Conditions

Parameter	Symbol	Min.	Max.	Unit	Note
Operating Temperature	$T_A$	-40	105	°C	a
Total Output Supply Voltage	$(V_{CC2} - V_{EE})$	15	30	V	b
Negative Output Supply Voltage	$(V_E - V_{EE})$	0	15	V	c
Positive Output Supply Voltage	$(V_{CC2} - V_E)$	15	$30 - (V_E - V_{EE})$	V	
Input Current (ON)	$I_{F(ON)}$	8	12	mA	
Input Voltage (OFF)	$V_{F(OFF)}$	-3.6	0.8	V	

- a. To achieve the absolute maximum power dissipation specified, pins 4, 9, and 10 require ground plane connections and might require airflow. See the Thermal Model section for details about how to estimate junction temperature and power dissipation. In most cases, the absolute maximum output IC junction temperature is the limiting factor. The actual power dissipation achievable will depend on the application environment (PCB layout, airflow, part placement, and so on). See the Recommended PCB Layout section for layout considerations. Output IC power dissipation is derated linearly at 10 mW/°C above 90°C. Input IC power dissipation does not require derating.
- b. 15V is the recommended minimum operating positive supply voltage ( $V_{CC2} - V_E$ ) to ensure adequate margin in excess of the maximum  $V_{UVLO+}$  threshold of 12.5V. For High Level Output Voltage testing,  $V_{OH}$  is measured with a dc load current. When driving capacitive loads,  $V_{OH}$  will approach  $V_{CC}$  as  $I_{OH}$  approaches zero units.
- c. This supply is optional. Required only when negative gate drive is implemented.

## Electrical Specifications (DC)

Unless otherwise noted, all typical values at  $T_A = 25^\circ\text{C}$ ,  $V_{CC2} - V_{EE} = 30\text{V}$ ,  $V_E - V_{EE} = 0\text{V}$ ; all minimum and maximum specifications are at recommended operating conditions.

Parameter	Symbol	Min.	Typ.	Max.	Unit	Test Conditions	Fig.	Note
FAULT Logic Low Output Voltage	$V_{\overline{\text{FAULT}}L}$	—	0.1	0.4	V	$I_{\overline{\text{FAULT}}} = 1.1\text{ mA}$ , $V_{CC1} = 5.5\text{V}$		
		—	0.1	0.4	V	$I_{\overline{\text{FAULT}}} = 1.1\text{ mA}$ , $V_{CC1} = 3.3\text{V}$		
FAULT Logic High Output Current	$I_{\overline{\text{FAULT}}H}$	—	0.02	0.5	μA	$V_{\overline{\text{FAULT}}} = 5.5\text{V}$ , $V_{CC1} = 5.5\text{V}$		
		—	0.002	0.3	μA	$V_{\overline{\text{FAULT}}} = 3.3\text{V}$ , $V_{CC1} = 3.3\text{V}$		
High Level Output Current	$I_{OH}$	-0.3	-0.75	—	A	$V_O = V_{CC2} - 4$	4, 18	a
		-1.0	—	—		$V_O = V_{CC2} - 15$		b
Low Level Output Current	$I_{OL}$	0.3	0.75	—	A	$V_O = V_{EE} + 2.5$	5, 19	a
		1.0	—	—		$V_O = V_{EE} + 15$		b
Low Level Output Current During Fault Condition	$I_{OLF}$	90	140	230	mA	$V_{OUT} - V_{EE} = 14\text{V}$		c
High Level Output Voltage	$V_{OH}$	$V_{CC} - 2.9$	$V_{CC} - 2.0$	—	V	$I_O = -650\text{ μA}$	2, 4, 20	d, e, f, g
Low Level Output Voltage	$V_{OL}$	—	0.17	0.5	V	$I_O = 100\text{ mA}$	3, 5, 21	
Clamp Pin Threshold Voltage	$V_{TH\_CLAMP}$	—	2.0	—	V			
Clamp Low Level Sinking Current	$I_{CLAMP}$	0.21	0.7	—	A	$V_O = V_{EE} + 2.5$		
High Level Supply Current	$I_{CC2H}$	—	2.5	5	mA	$I_O = 0\text{ mA}$	6, 7, 23	f
Low Level Supply Current	$I_{CC2L}$	—	2.5	5	mA	$I_O = 0\text{ mA}$		
Blanking Capacitor Charging Current	$I_{CHG}$	0.13	-0.24	-0.33	mA	$V_{DESAT} = 2\text{V}$	8, 24	f, h



Parameter	Symbol	Min.	Typ.	Max.	Unit	Test Conditions	Fig.	Note
Blanking Capacitor Discharge Current	$I_{DSCHG}$	10	30	—	mA	$V_{DESAT} = 7V$	25	
DESAT Threshold	$V_{DESAT}$	6	6.5	7.5	V	$V_{CC2} - V_E > V_{UVLO-}$	9, 27	f
UVLO Threshold	$V_{UVLO+}$	10.5	11.6	12.5	V	$V_O > 5V$		d, f, i
	$V_{UVLO-}$	9.2	10.3	11.1	V	$V_O < 5V$		d, f, j
UVLO Hysteresis	$(V_{UVLO+} - V_{UVLO-})$	0.4	1.3	—	V			
Threshold Input Current Low to High	$I_{FLH}$	—	2.0	6	mA	$I_O = 0 \text{ mA}, V_O > 5V$		
Threshold Input Voltage High to Low	$V_{FHL}$	0.8	—	—	V			
Input Forward Voltage	$V_F$	1.2	1.6	1.95	V	$I_F = 10 \text{ mA}$		
Temperature Coefficient of Input Forward Voltage	$\Delta V_F / \Delta T_A$	—	-1.3		mV/°C			
Input Reverse Breakdown Voltage	$BV_R$	5	—	—	V	$I_R = 10 \mu A$		
Input Capacitance	$C_{IN}$	—	70	—	pF	$f = 1 \text{ MHz}, V_F = 0V$		

- Maximum pulse width = 50  $\mu s$ .
- Maximum pulse width = 10  $\mu s$ . This value is intended to allow for component tolerances for designs with  $I_O$  peak minimum = 1.0A. Derate linearly from 2.0A at +25°C to 1.5A at +105°C. This compensates for increased  $I_{OPEAK}$  due to changes in  $V_{OL}$  over temperature.
- See [Slow IGBT Gate Discharge during Fault Condition](#) for further details.
- 15V is the recommended minimum operating positive supply voltage ( $V_{CC2} - V_E$ ) to ensure adequate margin in excess of the maximum  $V_{UVLO+}$  threshold of 12.5V. For High Level Output Voltage testing,  $V_{OH}$  is measured with a dc load current. When driving capacitive loads,  $V_{OH}$  will approach  $V_{CC}$  as  $I_{OH}$  approaches zero units.
- Maximum pulse width = 1.0 ms.
- Once  $V_O$  of the ACPL-331J is allowed to go high ( $V_{CC2} - V_E > V_{UVLO+}$ ), the DESAT detection feature of the ACPL-331J will be the primary source of IGBT protection. The UVLO is needed to ensure DESAT is functional. Once  $V_{CC2}$  is increased from 0V to above  $V_{UVLO+}$ , DESAT will remain functional until  $V_{CC2}$  is decreased below  $V_{UVLO-}$ . Thus, the DESAT detection and UVLO features of the ACPL-331J work in conjunction to ensure constant IGBT protection.
- To clamp the output voltage at  $V_{CC} - 3 V_{BE}$ , a pull-down resistor between the output and  $V_{EE}$  is recommended to sink a static current of 650  $\mu A$  while the output is high. See [Output Pull-Down Resistor](#) if an output pull-down resistor is not used.
- See [DESAT Fault Detection Blanking Time](#) for further details.
- This is the *increasing* (that is, turn-on or *positive-going* direction) of  $V_{CC2} - V_E$ .
- This is the *decreasing* (that is, turn-off or *negative-going* direction) of  $V_{CC2} - V_E$ .

## Switching Specifications (AC)

Unless otherwise noted, all typical values at  $T_A = 25^\circ\text{C}$ ,  $V_{CC2} - V_{EE} = 30\text{V}$ ,  $V_E - V_{EE} = 0\text{V}$ , all minimum and maximum specifications are at recommended operating conditions.

Parameter	Symbol	Min.	Typ.	Max.	Unit	Test Conditions	Fig.	Note
Propagation Delay Time to High Output Level	$t_{PLH}$	100	180	250	ns	$R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $f = 10\text{ kHz}$ , Duty Cycle = 50%, $I_F = 10\text{ mA}$ , $V_{CC2} = 30\text{V}$	1, 10, 11, 12, 13, 26	a, b
Propagation Delay Time to Low Output Level	$t_{PHL}$	100	180	250	ns			
Pulse Width Distortion	PWD	-100	20	100	ns			c, d
Propagation Delay Difference Between Any Two Parts or Channels	$(t_{PHL} - t_{PLH})$ PDD	-150	—	150	ns			d, e
Rise Time	$t_R$	—	50	—	ns			
Fall Time	$t_F$	—	50	—	ns			
DESAT Sense to 90% $V_O$ Delay	$t_{DESAT(90\%)}$	—	0.15	0.3	$\mu\text{s}$	$C_{DESAT} = 100\text{ pF}$ , $R_F = 2.1\text{ k}\Omega$ ,	14, 27, 34	f
DESAT Sense to 10% $V_O$ Delay	$t_{DESAT(10\%)}$	—	1.1	1.5	$\mu\text{s}$	$R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $V_{CC2} = 30\text{V}$		15, 16, 17, 27, 34
DESAT Sense to Low Level FAULT Signal Delay	$t_{DESAT(FAULT)}$	—	0.25	0.5	$\mu\text{s}$	$C_{DESAT} = 100\text{ pF}$ , $R_F = 2.1\text{ k}\Omega$ , $C_F = \text{Open}$ , $R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $V_{CC2} = 30\text{V}$	27, 34	g
		—	0.8	—	$\mu\text{s}$	$C_{DESAT} = 100\text{ pF}$ , $R_F = 2.1\text{ k}\Omega$ , $C_F = 1\text{ nF}$ , $R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $V_{CC2} = 30\text{V}$		
DESAT Sense to DESAT Low Propagation Delay	$t_{DESAT(LOW)}$	—	0.25	—	$\mu\text{s}$	$C_{DESAT} = 100\text{ pF}$ , $R_F = 2.1\text{ k}\Omega$ , $R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $V_{CC2} = 30\text{V}$	27, 34	f
DESAT Input Mute	$t_{DESAT(MUTE)}$	5	—	—	$\mu\text{s}$	$C_{DESAT} = 100\text{ pF}$ , $R_F = 2.1\text{ k}\Omega$ , $R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $V_{CC1} = 5.5\text{V}$ , $V_{CC2} = 30\text{V}$	34	h
RESET to High Level FAULT Signal Delay	$t_{RESET(FAULT)}$	0.3	1	2.0	$\mu\text{s}$	$C_{DESAT} = 100\text{ pF}$ , $R_F = 2.1\text{ k}\Omega$ , $R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $V_{CC1} = 5.5\text{V}$ , $V_{CC2} = 30\text{V}$		
		0.8	1.5	2.5	$\mu\text{s}$	$C_{DESAT} = 100\text{ pF}$ , $R_F = 2.1\text{ k}\Omega$ , $R_G = 20\Omega$ , $C_G = 5\text{ nF}$ , $V_{CC1} = 3.3\text{V}$ , $V_{CC2} = 30\text{V}$		

Parameter	Symbol	Min.	Typ.	Max.	Unit	Test Conditions	Fig.	Note
Output High Level Common Mode Transient Immunity	$ CM_H $	15	25	—	kV/ $\mu$ s	$T_A = 25^\circ\text{C}$ , $I_F = 10\text{ mA}$ , $V_{CM} = 1500\text{V}$ , $V_{CC2} = 30\text{V}$ , $R_F = 2.1\text{ k}\Omega$ , $C_F = 15\text{ nF}$	28, 29, 30, 31	i
		50	60	—		$T_A = 25^\circ\text{C}$ , $I_F = 10\text{ mA}$ , $V_{CM} = 1500\text{V}$ , $V_{CC2} = 30\text{V}$ , $R_F = 2.1\text{ k}\Omega$ , $C_F = 1\text{ nF}$		i, j
Output Low Level Common Mode Transient Immunity	$ CM_L $	15	25	—	kV/ $\mu$ s	$T_A = 25^\circ\text{C}$ , $V_F = 0\text{V}$ , $V_{CM} = 1500\text{V}$ , $V_{CC2} = 30\text{V}$ , $R_F = 2.1\text{ k}\Omega$ , $C_F = 15\text{ nF}$	28, 29, 30, 31	k
		50	60	—		$T_A = 25^\circ\text{C}$ , $V_F = 0\text{V}$ , $V_{CM} = 1500\text{V}$ , $V_{CC2} = 30\text{V}$ , $R_F = 2.1\text{ k}\Omega$ , $C_F = 1\text{ nF}$		

- This load condition approximates the gate load of a 1200V/75A IGBT.
- As measured from  $I_F$  to  $V_O$ .
- Pulse Width Distortion (PWD) is defined as  $|t_{PHL} - t_{PLH}|$  for any given unit.
- As measured from ANODE, CATHODE of LED to  $V_{OUT}$ .
- The difference between  $t_{PHL}$  and  $t_{PLH}$  between any two ACPL-331J parts under the same test conditions.
- The amount of time the DESAT threshold must be exceeded before  $V_{OUT}$  and the FAULT output begin to go low. This is supply voltage dependent.
- The amount of time from when the DESAT threshold is exceeded until the FAULT output goes low.
- FAULT Reset: The amount of time when  $V_{OUT}$  will be asserted low after the DESAT threshold is exceeded. See [FAULT Reset](#).
- Common mode transient immunity in the high state is the maximum tolerable  $dV_{CM}/dt$  of the common mode pulse,  $V_{CM}$ , to ensure that the output will remain in the high state (that is,  $V_O > 15\text{V}$  or FAULT  $> 2\text{V}$ ).
- Split resistors network with a ratio of 1:1 is needed at input LED1. See [Figure 31](#).
- Common mode transient immunity in the low state is the maximum tolerable  $dV_{CM}/dt$  of the common mode pulse,  $V_{CM}$ , to ensure that the output will remain in a low state (that is,  $V_O < 1.0\text{V}$  or FAULT  $< 0.8\text{V}$ ).

## Package Characteristics

Parameter	Symbol	Min.	Typ.	Max.	Unit	Test Conditions	Fig.	Note
Input-Output Momentary Withstand Voltage	$V_{ISO}$	5000	—	—	$V_{RMS}$	$RH < 50\%$ , $t = 1\text{ minute}$ , $T_A = 25^\circ\text{C}$		a, b
Input-Output Resistance	$R_{I-O}$	—	$>10^9$	—	$\Omega$	$V_{I-O} = 500\text{V}$		b
Input-Output Capacitance	$C_{I-O}$	—	1.3	—	pF	Frequency = 1 MHz		

- In accordance with UL 1577, each optocoupler is proof tested by applying an insulation test voltage  $\geq 6000 V_{RMS}$  for 1 second. This test is performed before the 100% production test for partial discharge (method b) shown in [IEC/EN/DIN EN60747-5-5 Insulation Characteristics](#).
- This is a two-terminal measurement: pins 1 to 8 are shorted together, and pins 9 to 16 are shorted together.

Figure 1:  $V_{OUT}$  Propagation Delay Waveforms

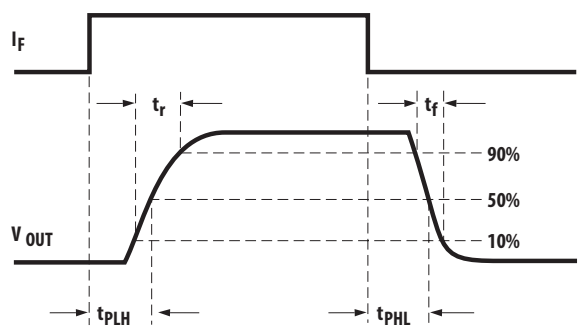


Figure 2:  $V_{OH}$  vs. Temperature

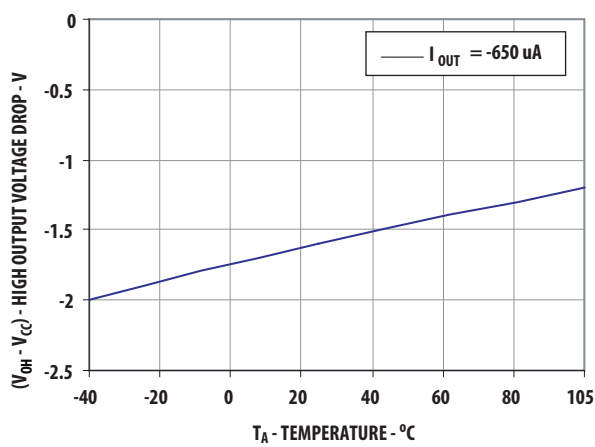


Figure 3:  $V_{OL}$  vs. Temperature

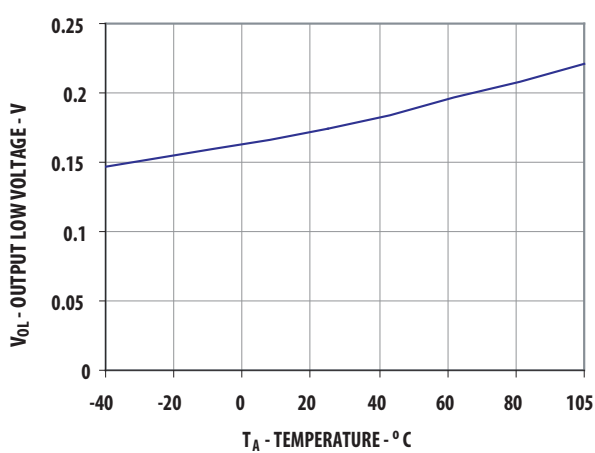


Figure 4:  $V_{OH}$  vs.  $I_{OH}$

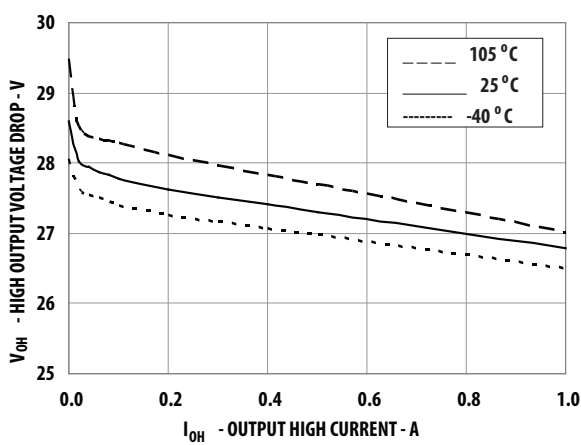


Figure 5:  $V_{OL}$  vs.  $I_{OL}$

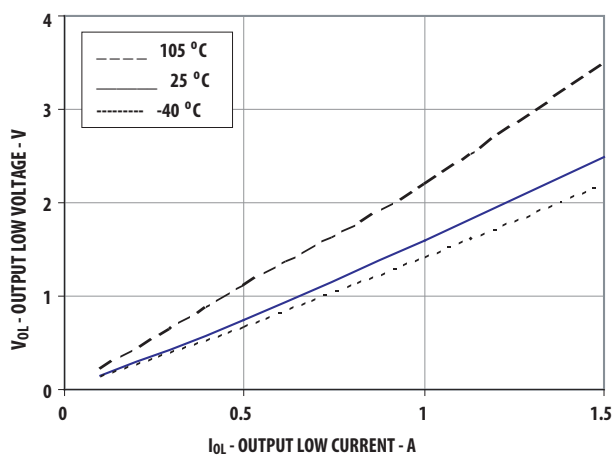


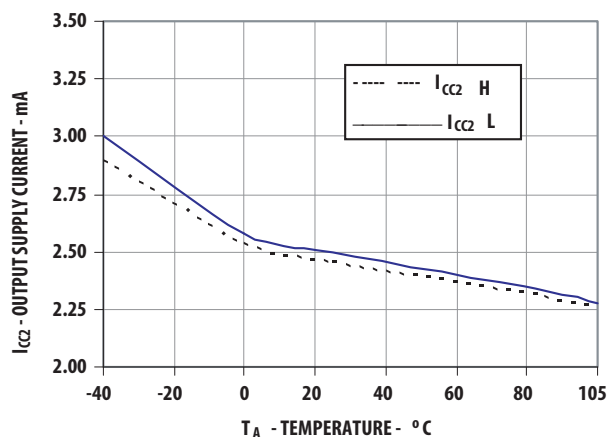
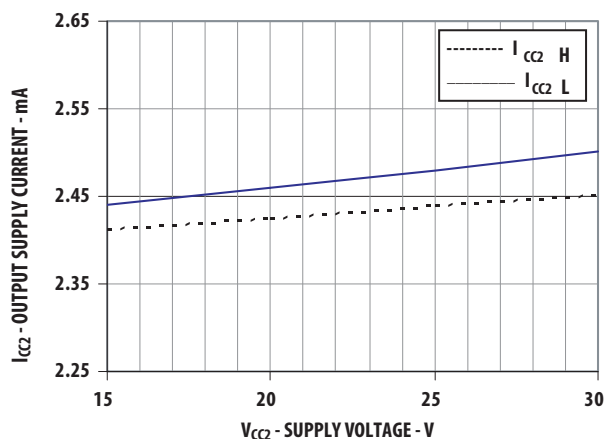
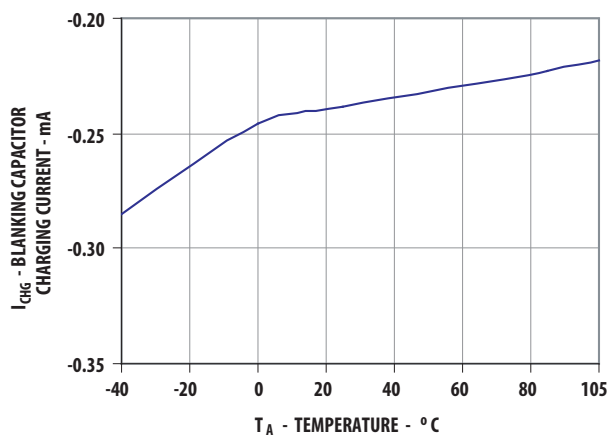
Figure 6:  $I_{CC2}$  vs. TemperatureFigure 7:  $I_{CC2}$  vs.  $V_{CC2}$ Figure 8:  $I_{CHG}$  vs. Temperature

Figure 9: DESAT Threshold vs. Temperature

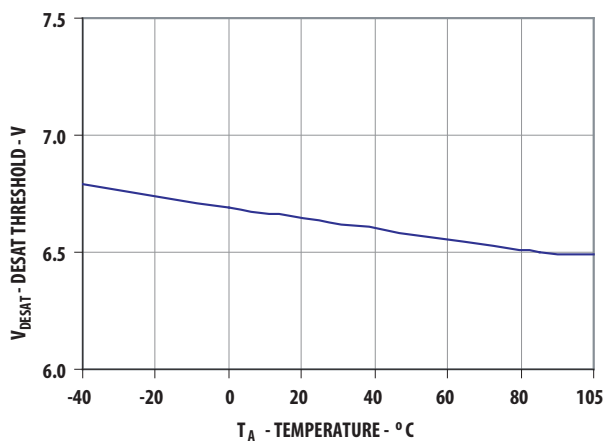


Figure 10: Propagation Delay vs. Temperature

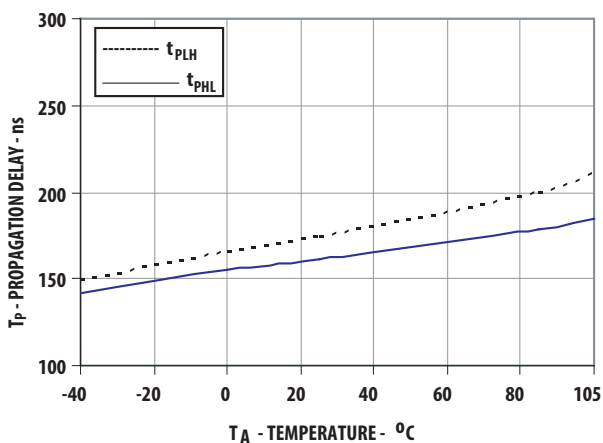


Figure 11: Propagation Delay vs. Supply Voltage

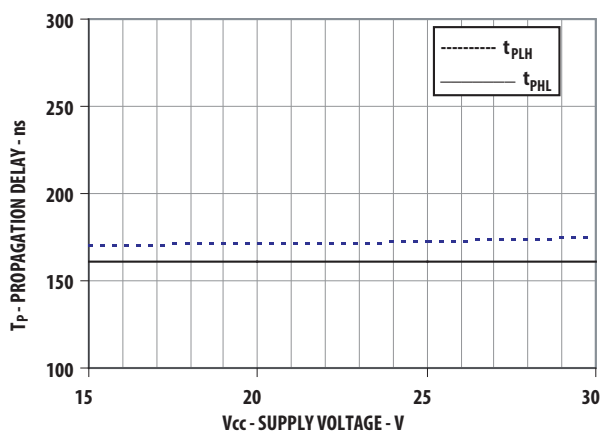


Figure 12: Propagation Delay vs. Load Resistance

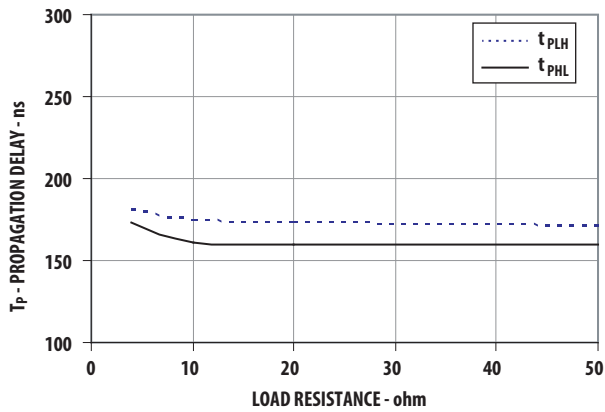
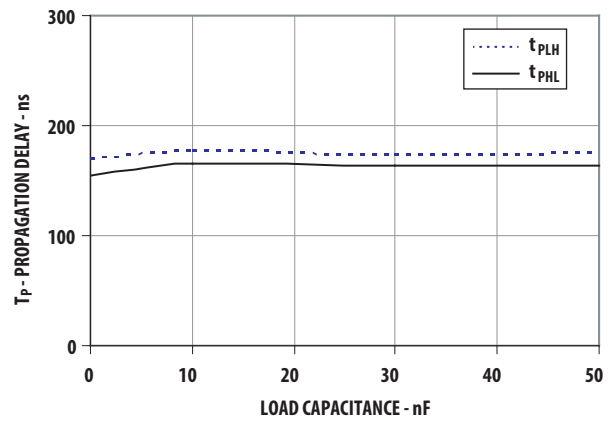
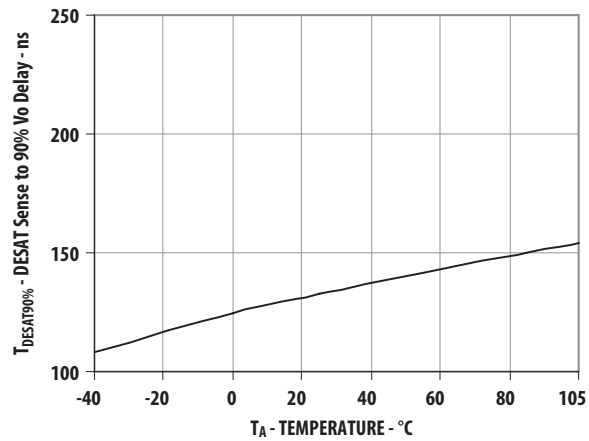
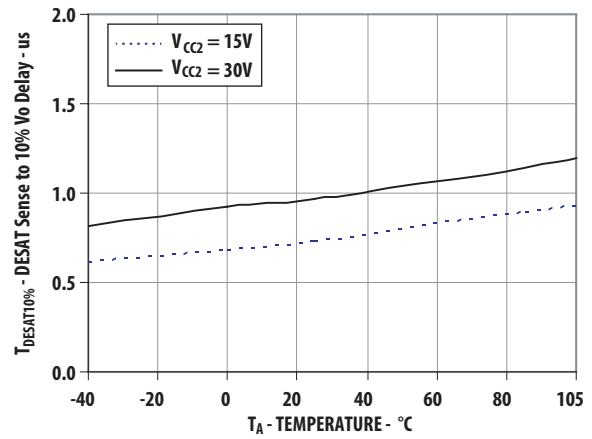
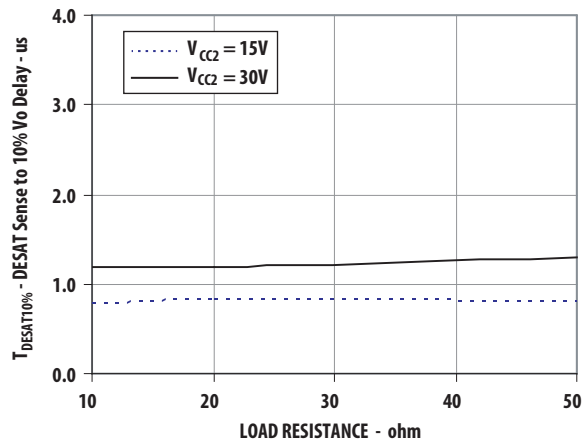
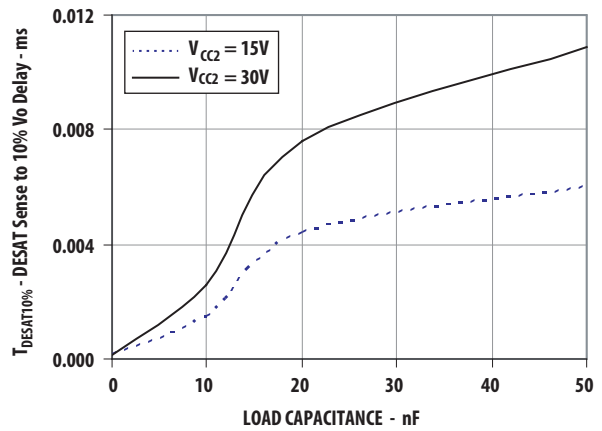
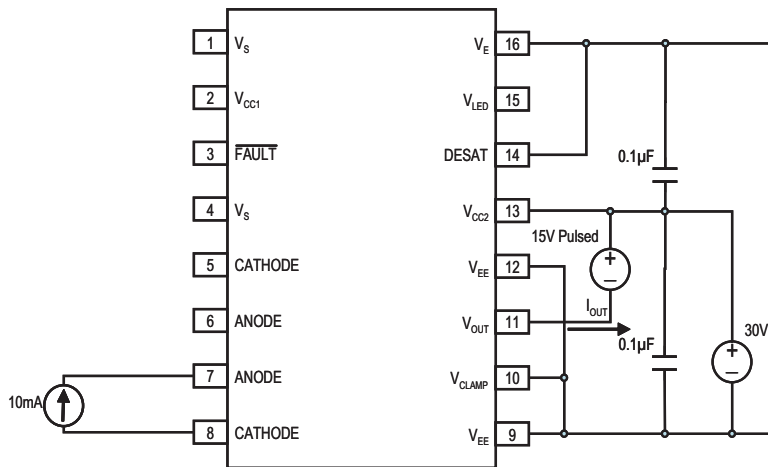
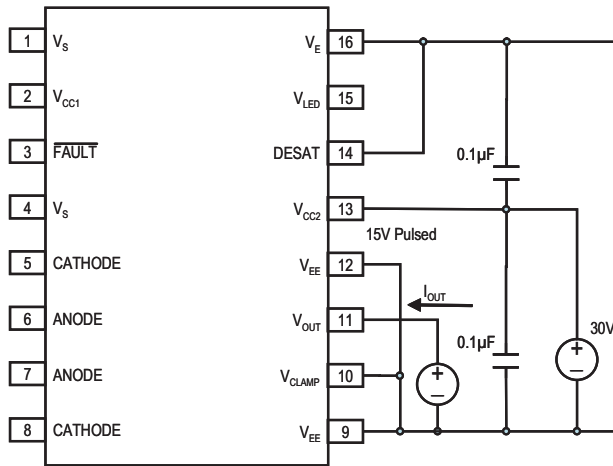
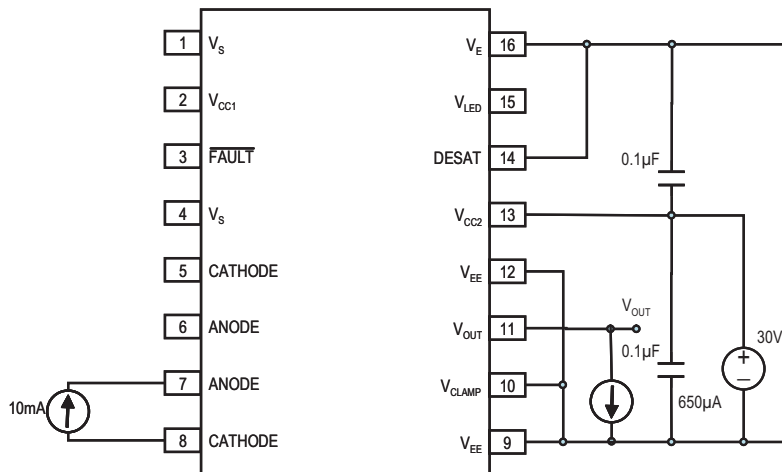
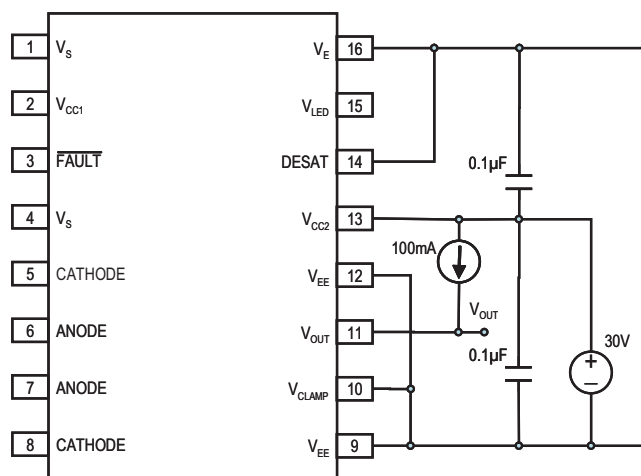
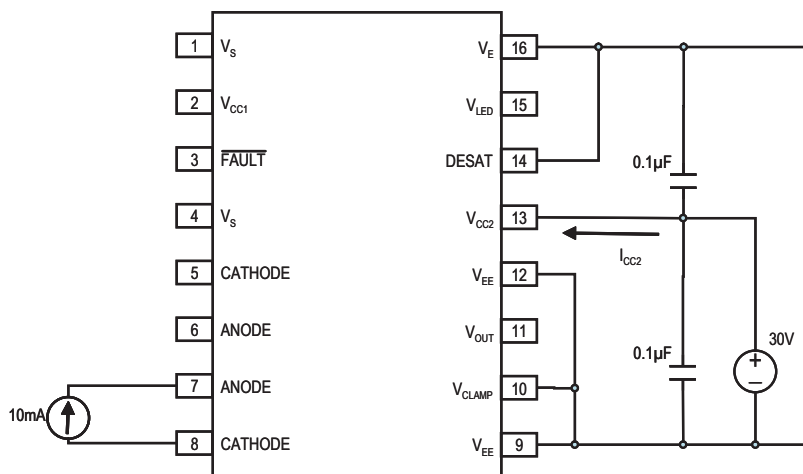
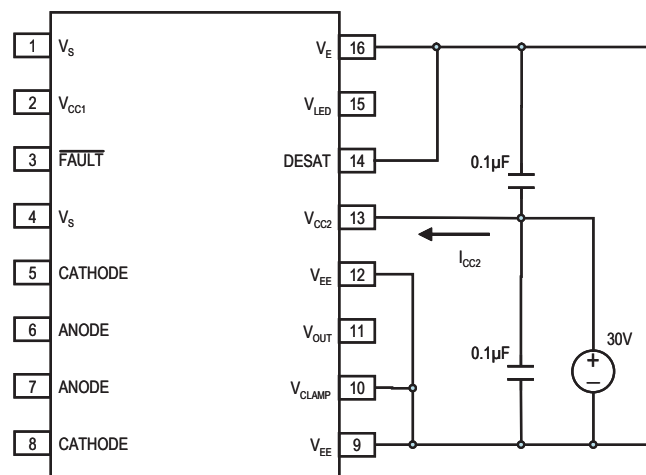


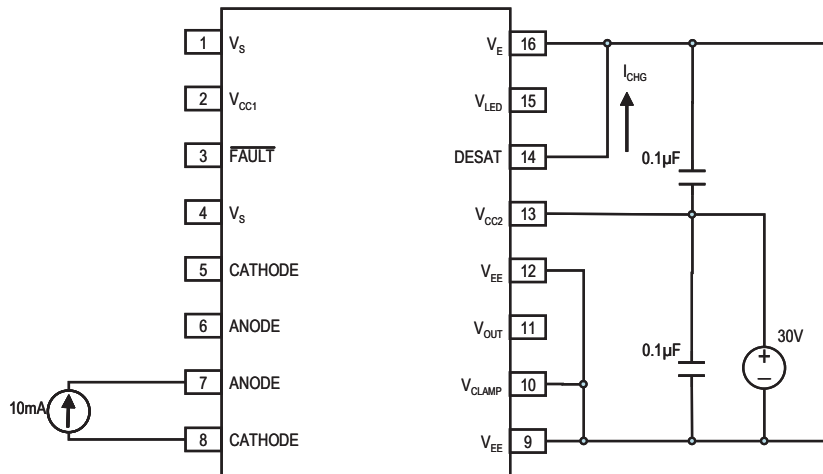
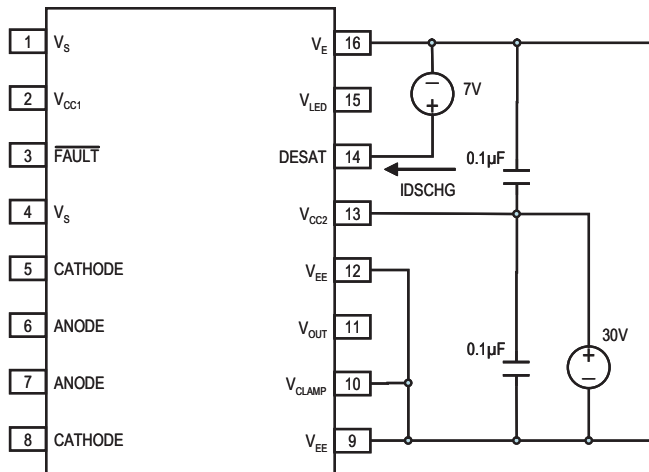
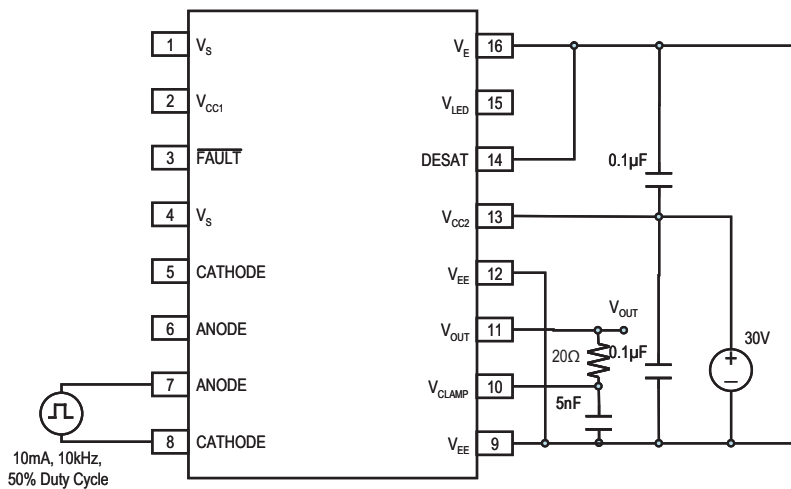
Figure 13: Propagation Delay vs. Load Capacitance

Figure 14: DESAT Sense to 90%  $V_{OUT}$  Delay vs. TemperatureFigure 15: DESAT Sense to 10%  $V_{OUT}$  Delay vs. TemperatureFigure 16: DESAT Sense to 10%  $V_{OUT}$  Delay vs. Load ResistanceFigure 17: DESAT Sense to 10%  $V_{OUT}$  Delay vs. Load Capacitance

**Figure 18:  $I_{OH}$  Pulsed Test Circuit****Figure 19:  $I_{OL}$  Pulsed Test Circuit****Figure 20:  $V_{OH}$  Pulsed Test Circuit**

**Figure 21:  $V_{OL}$  Pulsed Test Circuit****Figure 22:  $I_{CC2H}$  Test Circuit****Figure 23:  $I_{CC2L}$  Test Circuit**



**Figure 24:  $I_{CHG}$  Pulsed Test Circuit****Figure 25:  $I_{DSCHG}$  Test Circuit****Figure 26:  $t_{PLH}$ ,  $t_{PHL}$ ,  $t_f$ ,  $t_r$  Test Circuit**

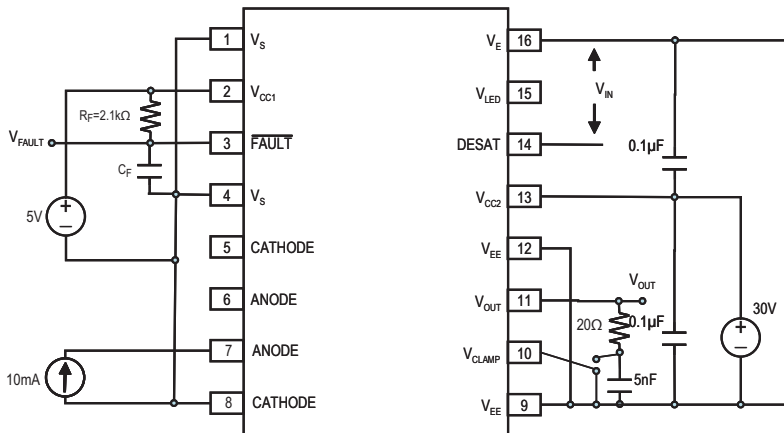
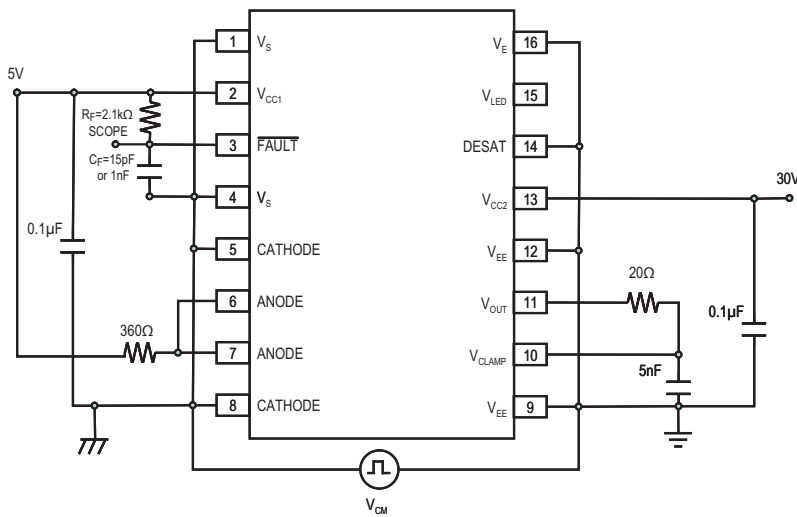
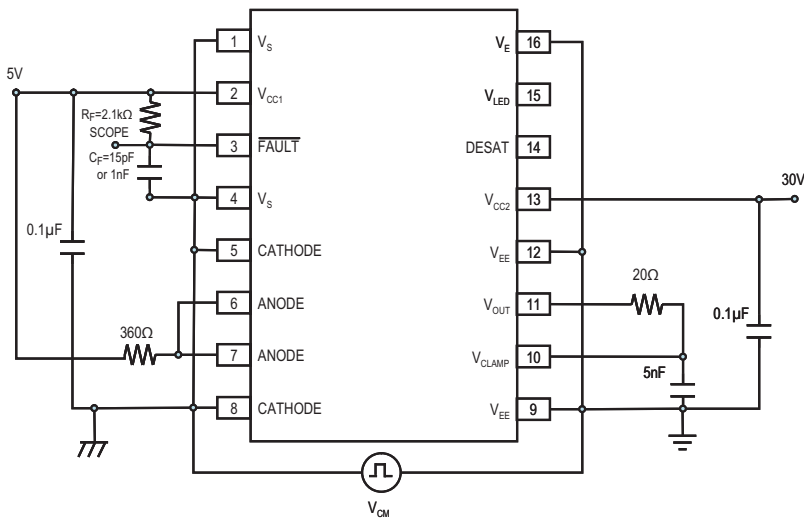
**Figure 27:  $t_{DESAT}$  Fault Test Circuit****Figure 28: CMR Test Circuit LED2 Off****Figure 29: CMR Test Circuit LED2 On**

Figure 30: CMR Test Circuit LED1 Off

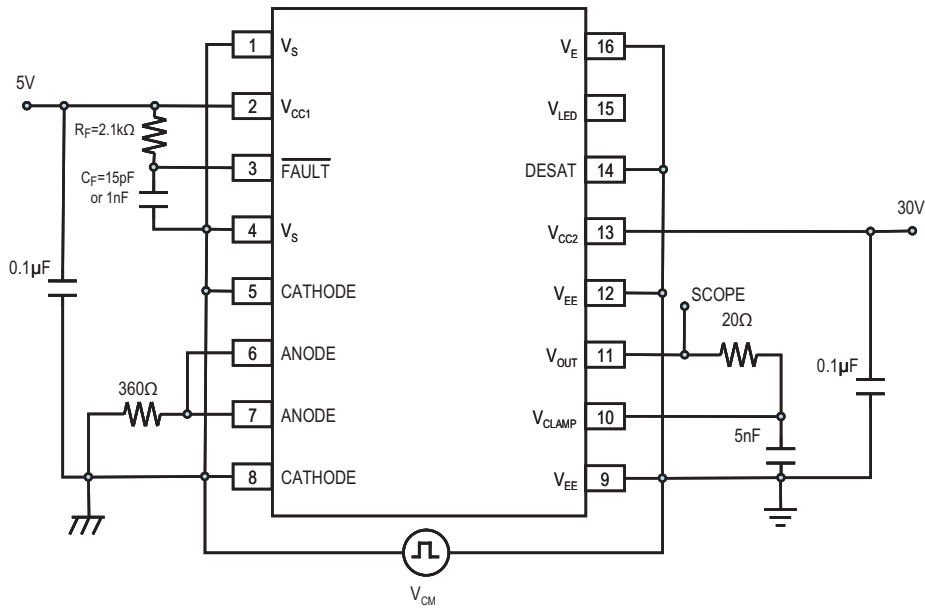
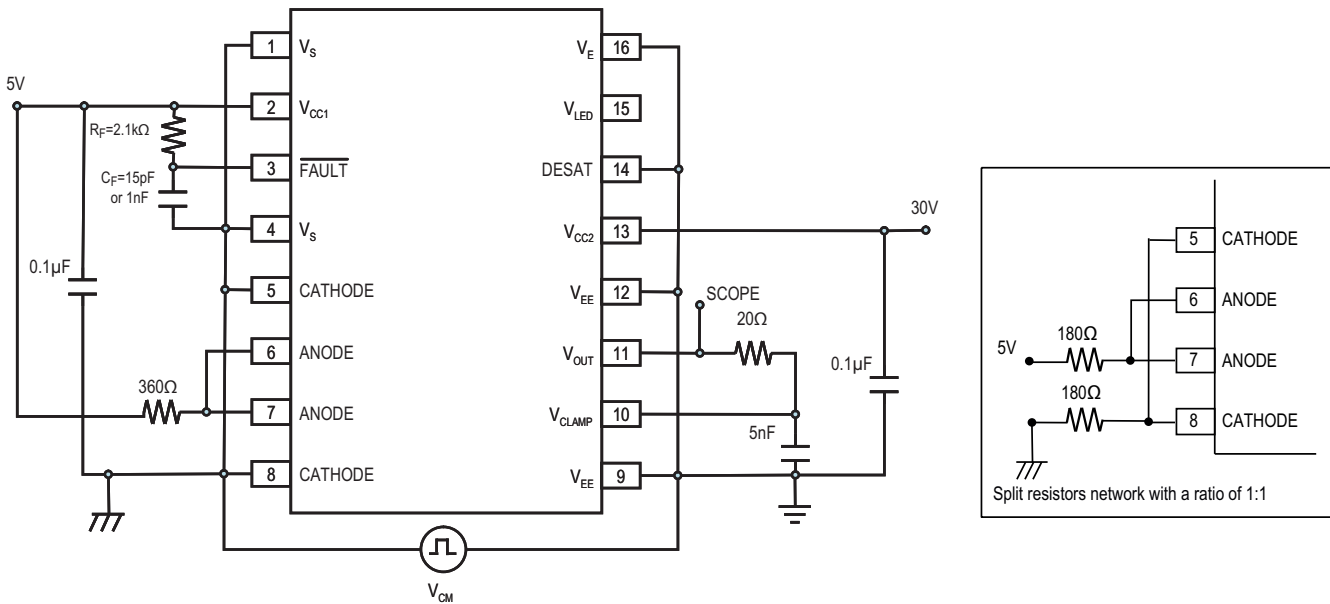


Figure 31: CMR Test Circuit LED1 On



## Application Information

### Product Overview Description

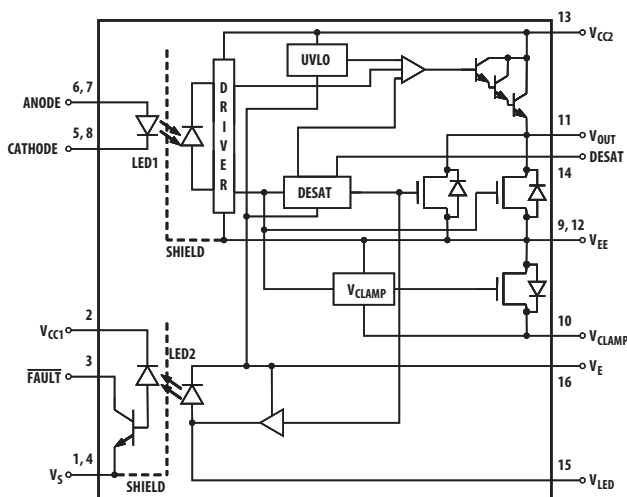
The ACPL-331J is a highly integrated power control device that incorporates all the necessary components for a complete, isolated IGBT/MOSFET gate drive circuit with fault protection and feedback into one SO-16 package. The active Miller clamp function eliminates the need for a negative gate drive in most applications and allows the use of a simple bootstrap supply for a high side driver. An optically isolated power output stage drives IGBTs with power ratings of up to 100A and 1200V. A high-speed internal optical link minimizes the propagation delays between the microcontroller and the IGBT while allowing the two systems to operate at very large common mode voltage differences that are common in industrial motor drives and other power switching applications. An output IC provides local protection for the IGBT to prevent damage during overcurrent, and a second optical link provides a fully isolated fault status feedback signal for the microcontroller. A built-in *watchdog* circuit, UVLO, monitors the power stage supply voltage to prevent IGBT caused by insufficient gate drive voltages. This integrated IGBT gate driver is designed to increase the performance and reliability of a motor drive without the cost, size, and complexity of a discrete design.

Two light-emitting diodes and two integrated circuits housed in the same SO-16 package provide the input control circuitry, the output power stage, and two optical channels. The output Detector IC is designed and manufactured on a high-voltage BiCMOS/Power DMOS process. The forward optical signal path, as indicated by LED1, transmits the gate control signal. The return optical signal path, as indicated by LED2, transmits the fault status feedback signal.

Under normal operation, the LED1 directly controls the IGBT gate through the isolated output detector IC, and LED2 remains off. When an IGBT fault is detected, the output detector IC immediately begins a *soft* shutdown sequence, reducing the IGBT current to zero in a controlled manner to avoid potential IGBT damage from inductive overvoltages. Simultaneously, this fault status is transmitted back to the input via LED2, where the fault latch disables the gate control input and the active low fault output alerts the microcontroller.

During power-up, the under-voltage lockout (UVLO) feature prevents the application of insufficient gate voltage to the IGBT by forcing the ACPL-331J's output low. Once the output is in the high state, the DESAT ( $V_{CE}$ ) detection feature of the ACPL-331J provides IGBT protection. Thus, UVLO and DESAT work in conjunction to provide constant IGBT protection.

Figure 32: Block Diagram of ACPL-331J

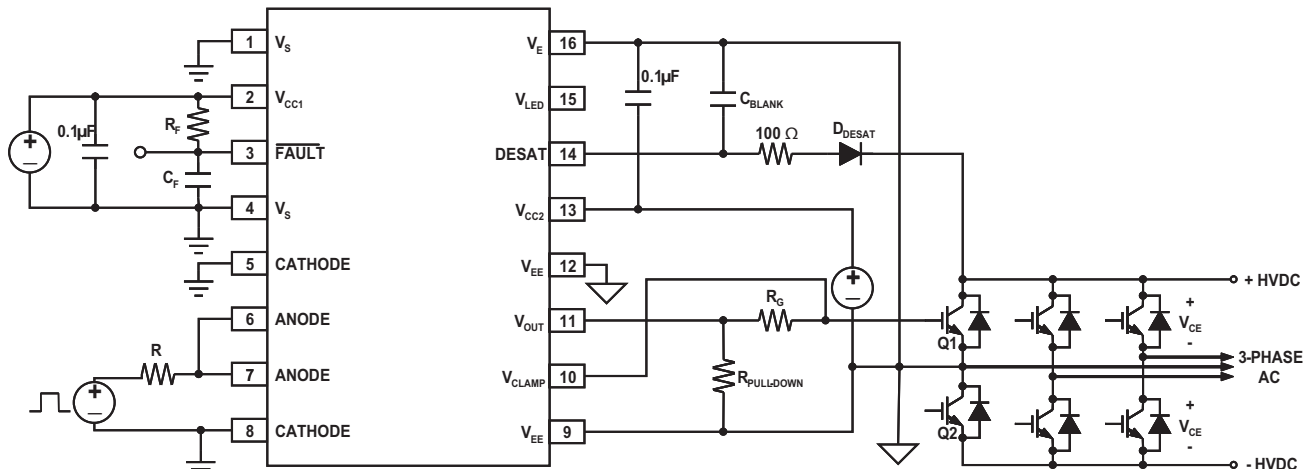


### Recommended Application Circuit

The ACPL-331J has an LED input gate control, and an open collector fault output suitable for wired-OR applications. The recommended application circuit shown in [Figure 33](#) illustrates a typical gate drive implementation using the ACPL-331J. The application circuit describes the driving of the IGBT. However, it is also applicable to the MOSFET. Depending upon the MOSFET or IGBT gate threshold requirements, you may want to adjust the  $V_{CC}$  supply voltage ( $V_{CC} = 17.5V$  for the IGBT and 12.5V for the MOSFET is recommended).

The two supply bypass capacitors ( $0.1\ \mu\text{F}$ ) provide the large transient currents necessary during a switching transition. Because of the transient nature of the charging currents, a low current (5 mA) power supply suffices. The desaturation diode  $D_{\text{DESAT}}$  600V/1200V fast recovery type,  $t_{\text{rr}}$  below 75 ns (for example, ERA34-10), and capacitor  $C_{\text{BLANK}}$  are necessary external components for the fault detection circuitry. The gate resistor  $R_G$  serves to limit gate charge current and controls the IGBT collector voltage rise and fall times. The open collector fault output has a passive pull-up resistor  $R_F$  ( $2.1\ \text{k}\Omega$ ) and a 1000-pF filtering capacitor,  $C_F$ . A 47-k $\Omega$  pull-down resistor  $R_{\text{PULL-DOWN}}$  on  $V_{\text{OUT}}$  provides a predictable high level output voltage ( $V_{\text{OH}}$ ). In this application, the IGBT gate driver will shut down when a fault is detected and the fault is reset by the next cycle of IGBT turn-on. See [Related Application Notes](#).

**Figure 33: Recommended Application Circuit (Single Supply) with Desaturation Detection and Active Miller Clamp**



## Description of Operation

### Normal Operation

During normal operation,  $V_{\text{OUT}}$  of the ACPL-331J is controlled by the input LED current  $I_F$  (pins 5, 6, 7, and 8), with the IGBT collector-to-emitter voltage being monitored through DESAT. The FAULT output is high. See [Figure 34](#).

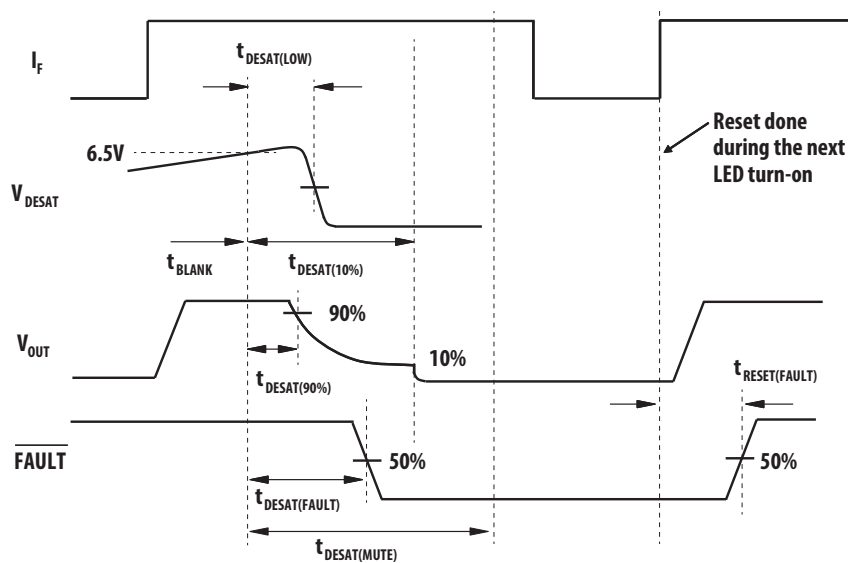
### Fault Condition

The DESAT pin monitors the IGBT  $V_{\text{CE}}$  voltage. When the voltage on the DESAT pin exceeds 6.5V while the IGBT is on,  $V_{\text{OUT}}$  is slowly brought low in order to *softly* turn off the IGBT and prevent large  $di/dt$  induced voltages. Also activated is an internal feedback channel that brings the FAULT output low for the purpose of notifying the microcontroller of the fault condition.

### FAULT Reset

Once the fault is detected, the output will be muted for  $5\ \mu\text{s}$  (minimum). All input LED signals will be ignored during the mute period to allow the driver to completely soft shut down the IGBT. The fault mechanism can be reset by the next LED turn-on after the  $5\ \mu\text{s}$  (minimum) mute time. See [Figure 34](#).

Figure 34: Fault Timing Diagram



## Output Control

The outputs ( $V_{OUT}$  and  $FAULT$ ) of the ACPL-331J are controlled by the combination of  $I_F$ , UVLO, and a detected IGBT DESAT condition. Once UVLO is not active ( $V_{CC2} - V_E > V_{UVLO}$ ),  $V_{OUT}$  is allowed to go high, and the DESAT (pin 14) detection feature of the ACPL-331J will be the primary source of IGBT protection. Once  $V_{CC2}$  is increased from 0V to above  $V_{UVLO+}$ , DESAT will remain functional until  $V_{CC2}$  is decreased below  $V_{UVLO-}$ . Thus, the DESAT detection and UVLO features of the ACPL-331J work in conjunction to ensure constant IGBT protection.

## Desaturation Detection and High Current Protection

The ACPL-331J satisfies these criteria by combining a high-speed, high output current driver, high-voltage optical isolation between the input and output, local IGBT desaturation detection and shutdown, and an optically isolated fault status feedback signal into a single 16-pin surface-mount package.

The fault detection method, which is adopted in the ACPL-331J, is to monitor the saturation (collector) voltage of the IGBT and to trigger a local fault shutdown sequence if the collector voltage exceeds a predetermined threshold. A small gate discharge device slowly reduces the high short circuit IGBT current to prevent damaging voltage spikes.

Before the dissipated energy can reach destructive levels, the IGBT is shut off. During the off state of the IGBT, the fault detect circuitry is simply disabled to prevent false *fault* signals.

The alternative protection scheme of measuring IGBT current to prevent desaturation is effective if the short circuit capability of the power device is known, but this method will fail if the gate drive voltage decreases enough to only partially turn on the IGBT. By directly measuring the collector voltage, the ACPL-331J limits the power dissipation in the IGBT even with insufficient gate drive voltage. Another more subtle advantage of the desaturation detection method is that power dissipation in the IGBT is monitored, while the current sense method relies on a preset current threshold to predict the safe limit of operation. Therefore, an overly conservative overcurrent threshold is not needed to protect the IGBT.

## Slow IGBT Gate Discharge during Fault Condition

When a desaturation fault is detected, a weak pull-down device in the ACPL-331J output drive stage will turn on to *softly* turn off the IGBT. This device slowly discharges the IGBT gate to prevent fast changes in drain current that could cause damaging voltage spikes due to lead and wire inductance. During the slow turn off, the large output pull-down device remains off until the output voltage falls below  $V_{EE} + 2V$ , at which time the large pull-down device clamps the IGBT gate to  $V_{EE}$ .

## DESAT Fault Detection Blanking Time

The DESAT fault detection circuitry must remain disabled for a short time period following the turn-on of the IGBT to allow the collector voltage to fall below the DESAT threshold. This time period, called the DESAT blanking time, is controlled by the internal DESAT charge current, the DESAT voltage threshold, and the external DESAT capacitor.

The nominal blanking time is calculated in terms of external capacitance ( $C_{BLANK}$ ), FAULT threshold voltage ( $V_{DESAT}$ ), and DESAT charge current ( $I_{CHG}$ ) as  $t_{BLANK} = C_{BLANK} \times V_{DESAT}/I_{CHG}$ . The nominal blanking time with the recommended 100-pF capacitor is  $100 \text{ pF} \times 6.5\text{V}/240 \text{ }\mu\text{A} = 2.7 \text{ }\mu\text{s}$ .

The capacitance value can be scaled slightly to adjust the blanking time, though a value smaller than 100 pF is not recommended. This nominal blanking time represents the longest time it will take for the ACPL-331J to respond to a DESAT fault condition. If the IGBT is turned on while the collector and emitter are shorted to the supply rails (switching into a short), the soft shutdown sequence will begin after approximately 3  $\mu\text{s}$ . If the IGBT collector and emitter are shorted to the supply rails after the IGBT is already on, the response time will be much quicker due to the parasitic parallel capacitance of the DESAT diode. The recommended 100-pF capacitor should provide adequate blanking as well as fault response times for most applications.

$I_F$	UVLO ( $V_{CC2} - V_E$ )	DESAT Function	Pin 3 (FAULT) Output	$V_{OUT}$
ON	Active	Not Active	High	Low
ON	Not Active	Active (with DESAT fault)	Low (FAULT)	Low
ON	Not Active	Active (no DESAT fault)	High (or no fault)	High
OFF	Active	Not Active	High	Low
OFF	Not Active	Not Active	High	Low

## Under-Voltage Lockout

The Under-Voltage Lockout (UVLO) feature is designed to prevent the application of insufficient gate voltage to the IGBT by forcing the ACPL-331J output low during power-up. IGBTs typically require gate voltages of 15V to achieve their rated  $V_{CE(ON)}$  voltage. At gate voltages below 13V typically, the  $V_{CE(ON)}$  voltage increases dramatically, especially at higher currents. At very low gate voltages below 10V, the IGBT may operate in the linear region and quickly overheat. The UVLO function causes the output to be clamped whenever insufficient operating supply ( $V_{CC2}$ ) is applied. Once  $V_{CC2}$  exceeds  $V_{UVLO+}$  (the positive-going UVLO threshold), the UVLO clamp is released to allow the device output to turn on in response to input signals. As  $V_{CC2}$  is increased from 0V (at some level below  $V_{UVLO+}$ ), first the DESAT protection circuitry becomes active. As  $V_{CC2}$  is further increased (above  $V_{UVLO+}$ ), the UVLO clamp is released. Before the time the UVLO clamp is released, the DESAT protection is already active. Therefore, the UVLO and DESAT fault detection feature work together to provide seamless protection regardless of supply voltage ( $V_{CC2}$ ).

## Active Miller Clamp

A Miller clamp allows the control of the Miller current during a high dV/dt situation and can eliminate the use of a negative supply voltage in most of the applications. During turn-off, the gate voltage is monitored and the clamp output is activated when gate voltage goes below 2V (relative to  $V_{EE}$ ). The clamp voltage is  $V_{OL} + 2.5\text{V}$  typical for a Miller current up to 1100 mA. The clamp is disabled when the LED input is triggered again.

## Other Recommended Components

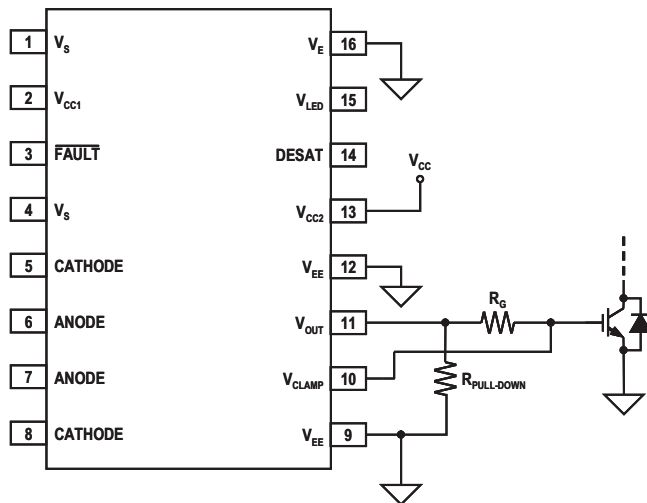
The application circuit in [Figure 33](#) includes an output pull-down resistor, a DESAT pin protection resistor, a FAULT pin capacitor, and a FAULT pin pull-up resistor and active Miller clamp connection.

## Output Pull-Down Resistor

During the output high transition, the output voltage rapidly rises to within 3 diode drops of  $V_{CC2}$ . If the output current then drops to zero due to a capacitive load, the output voltage will slowly rise from roughly  $V_{CC2} - 3(V_{BE})$  to  $V_{CC2}$  within a period of several microseconds. To limit the output voltage to  $V_{CC2} - 3(V_{BE})$ , a pull-down resistor,  $R_{PULL-DOWN}$ , between the output and  $V_{EE}$  is recommended to sink a static current of several 650  $\mu A$  while the output is high. Pull-down resistor values are dependent on the amount of positive supply and can be adjusted according to the formula,

$$R_{PULL-DOWN} = [V_{CC2} - 3 \times (V_{BE})] / 650 \mu A.$$

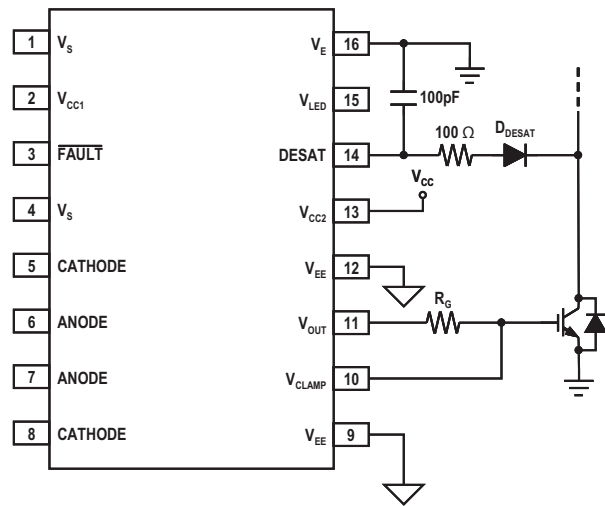
Figure 35: Output Pull-Down Resistor



## DESAT Pin Protection Resistor

The freewheeling of flyback diodes connected across the IGBTs can have large instantaneous forward voltage transients, which greatly exceed the nominal forward voltage of the diode. This may result in a large negative voltage spike on the DESAT pin, which will draw substantial current out of the driver if protection is not used. To limit this current to levels that will not damage the driver IC, a 100 $\Omega$  resistor should be inserted in series with the DESAT diode. The added resistance will not alter the DESAT threshold or the DESAT blanking time.

Figure 36: DESAT Pin Protection



## Capacitor on FAULT Pin for High CMR

Rapid common mode transients can affect the fault pin voltage while the fault output is in the high state. A 1000-pF capacitor should be connected between the fault pin and ground to achieve adequate CMOS noise margins at the specified CMR value of 50 kV/ $\mu s$ .

## Pull-Up Resistor on FAULT Pin

The FAULT pin is an open collector output and therefore requires a pull-up resistor to provide a high-level signal. Also, the FAULT output can be wire OR-ed together with other types of protection (for example, overtemperature, overvoltage, overcurrent) to alert the microcontroller.



**Figure 37: IGBT Drive with Negative Gate Drive, External Booster and Desaturation Detection**



- $V_{CLAMP}$  should be connected to  $V_{EE}$  when it is not used.
- $V_{CLAMP}$  is used as secondary gate discharge path.
- \* indicates component required for negative gate drive topology.

[illegible]

**NOTE:**

- $V_{CLAMP}$  control secondary discharge path for higher power application.
- \* indicates component required for negative gate drive topology.

## Thermal Model

The ACPL-331J is designed to dissipate the majority of the heat through pins 1 and 4 for the input IC and pins 9 and 12 for the output IC. (There are two  $V_{EE}$  pins on the output side, pins 9 and 12, for this purpose.) Heat flow through other pins or through the package directly into ambient are considered negligible and are not modeled here.

To achieve the power dissipation specified in the absolute maximum specification, it is imperative that pins 1, 4, 9, and 12 have ground planes connected to them. As long as the maximum power specification is not exceeded, the only other limitation to the amount of power one can dissipate is the absolute maximum junction temperature specification of 125°C. The junction temperatures can be calculated with the following equations:

$$T_{ji} = P_i (\theta_{i1} + \theta_{1A}) + T_A$$

$$T_{jo} = P_o (\theta_{o9,12} + \theta_{9,12A}) + T_A$$

where  $P_i$  = power into input IC and  $P_o$  = power into output IC. Since  $\theta_{1A}$  and  $\theta_{9,12A}$  are dependent on PCB layout and airflow, their exact number may not be available.

Therefore, a more accurate method of calculating the junction temperature is with the following equations:

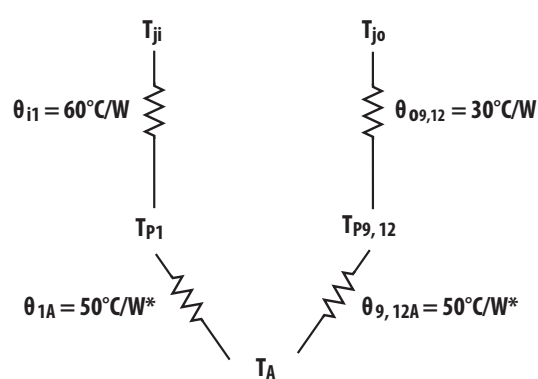
$$T_{ji} = P_i \theta_{i1} + T_{P1}$$

$$T_{jo} = P_o \theta_{o9,12} + T_{P9,12}$$

These equations, however, require that the pin 1 and pins 9, 12 temperatures be measured with a thermal couple on the pin at the ACPL-331J package edge.

If the calculated junction temperatures for the thermal model in Figure 39 is higher than 125°C, the pin temperature for pins 9 and 12 should be measured (at the package edge) under worst-case operating environment for a more accurate estimate of the junction temperatures.

Figure 39: ACPL-331J Thermal Model



$T_{ji}$  = junction temperature of input side IC

$T_{jo}$  = junction temperature of output side IC

$T_{P1}$  = pin 1 temperature at package edge

$T_{P9,12}$  = pin 9 and 12 temperature at package edge

$\theta_{i1}$  = input side IC to pin 1 thermal resistance

$\theta_{o9,12}$  = output side IC to pin 9 and 12 thermal resistance

$\theta_{1A}$  = pin 1 to ambient thermal resistance

$\theta_{9,12A}$  = pin 9 and 12 to ambient thermal resistance

\*The  $\theta_{1A}$  and  $\theta_{9,12A}$  values shown here are for PCB layouts with reasonable air flow.

This value may increase or decrease by a factor of 2 depending on PCB layout and/or airflow.

## Related Application Notes

- Application Note 5314 – *Active Miller Clamp Application Note*
- Application Note 5324 – *Desaturation Fault Detection Application Note*
- Application Note 5315 – *"Soft" Turn-off Feature Application Note*
- Application Note 1043 – *Common-Mode Noise: Sources and Solutions Application Note*
- AN02-0310EN – *Plastics Optocoupler Products: ESD and Moisture Sensitivity Reliability Data Sheet*

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